Regulations Compliance Report

Approved Document L1A, 2013 Edition, England assessed by Stroma FSAP 2012 program, Version: 1.0.4.23 *Printed on 13 January 2020 at 15:45:13*

| Project Informatic | on: | | | |
|----------------------|---|--|-------------------------------|--------------------------|
| Assessed By: | Mitchel Armitage-N | leiles (STRO029948) | Building Type: | Mid-terrace House |
| Dwelling Details: | | | | |
| NEW DWELLING | DESIGN STAGE | | Total Floor Area: 8 | 2.76m ² |
| Site Reference : | Fishers Farm (Pha | se 2) | Plot Reference: | Plot 104 Dart [Mid] DCC3 |
| Address : | | | | |
| Client Details: | | | | |
| Name: | Redrow Homes Sc | outh East | | |
| Address : | | | | |
| • | s items included wi te report of regulat | thin the SAP calculations. ons compliance. | | |
| 1a TER and DER | 2 | | | |
| | ing system: Mains ga | as | | |
| Fuel factor: 1.00 (r | nains gas) oxide Emission Rate (| | 17.06 kg/m² | |
| - | Dioxide Emission Rate | | 15.75 kg/m² | ОК |
| 1b TFEE and DF | | - () | | |
| - | rgy Efficiency (TFEE | | 45.7 kWh/m ² | |
| Dwelling Fabric Er | nergy Efficiency (DFE | E) | 38.4 kWh/m ² | 01/ |
| 2 Fabric U-value | | | | OK |
| Element | 5 | Average | Highest | |
| External v | wall | 0.28 (max. 0.30) | 0.28 (max. 0.70) | ОК |
| Party wal | | 0.00 (max. 0.20) | - | OK |
| Floor | | 0.12 (max. 0.25) | 0.12 (max. 0.70) | ОК |
| Roof | | 0.11 (max. 0.20) | 0.11 (max. 0.35) | OK |
| Openings | | 1.29 (max. 2.00) | 1.50 (max. 3.30) | OK |
| 2a Thermal bridg | | | A 45 | |
| Reference | e: Measured | sing user-specified y-value of | 0.15 | |
| 3 Air permeabilit | | | E 01 (design vol | uo) |
| Maximum | oility at 50 pascals | | 5.01 (design valı 10.0 | OK |
| 4 Heating efficie | ncy | | | |
| Main Heatir | ng system: | Database: (rev 454, produc | t index 017929): | |
| | | Boiler systems with radiator Brand name: Ideal Model: LOGIC COMBI Model qualifier: ESP1 35 (Combi) Efficiency 89.6 % SEDBUK | rs or underfloor heating - ma | ains gas |
| | | Minimum 88.0 % | | ОК |

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| Secondary he | eating system: | None | | |
|------------------------------|----------------------------------|----------------------------|-----------------------|----|
| 5 Cylinder insulat | ion | | | |
| Hot water Sto | orage: | No cylinder | | |
| 6 Controls | | | | |
| | | | | |
| Space heatin | - | Programmer, room thermosta | at and TRVs | OK |
| Hot water cor | ntrols: | No cylinder thermostat | | |
| Boiler interloo | ·k· | No cylinder Yes | | ок |
| 7 Low energy ligh | | | | ON |
| | f fixed lights with lo | w-energy fittings | 100.0% | |
| Minimum | | | 75.0% | ОК |
| 8 Mechanical ven | tilation | | | |
| Not applicabl | е | | | |
| 9 Summertime ter | nperature | | | |
| Overheating | risk (South East En | gland): | Not significant | ОК |
| Based on: | | | | |
| Overshading | | | Average or unknown | |
| | ng: North West | | 4.76m² 3m² | |
| | ng: South East ng: South East | | 5.22m ² | |
| Ventilation ra | - | | 8.00 | |
| Blinds/curtain | | | None | |
| | | | | |
| 10 Key features | | | | |
| Doors U-valu | - | | 1.1 W/m²K | |
| Roofs U-valu | - | | 0.11 W/m²K | |
| Party Walls Floors U-valu | | | 0 W/m²K 0.12 W/m²K | |
| FIGUIS O-VAIU | C | | 0.12 W/III-R | |

Code for Sustainable Homes Report For use with Nov 2010 addendum 2014 England

| Assessor and House | Details | | | |
|-------------------------------------|-------------------------|------------------|------------|--|
| Assessor Name: Property Address: | Mitchel Armitage-Neiles | Assessor Number: | STRO029948 | |
| Buiding regulation as | sessment | | | |
| | | | kg/m²/year | |
| TER | | | 17.06 | |
| DER | | | 15.75 | |
| ENE 1 Assessment - | Dwelling Emission Rate | | | |

Total Energy Type CO₂ Emissions for Codes Levels 1 - 5

| | % | kg/m²/year | |
|--|-----|------------|-------|
| DER from SAP 2012 DER Worksheet | | 15.75 | (ZC1) |
| TER | | 17.06 | |
| Residual CO2 emissions offset from biofuel CHP | | 0 | (ZC5) |
| CO2 emissions offset from additional allowable electricty generation | | 0 | (ZC7) |
| Total CO2 emissions offset from SAP Section 16 allowances | | 0 | |
| DER accounting for SAP Section 16 allowances | | 15.75 | |
| % improvement DER/TER | 7.7 | | |

Total Energy Type CO2 Emissions for Codes Levels 6

| | kg/m²/year | |
|---|------------|-------|
| DER accounting for SAP Section 16 allowances | 15.75 | (ZC1) |
| CO2 emissions from appliances, equation (L14) | 16.06 | (ZC2) |
| CO2 emissions from cooking, equation (L16) | 2.17 | (ZC3) |
| Net CO2 emissions | 36 | (ZC8) |

Result:

Credits awarded for ENE 1 = 1.2

Code Level = 3

ENE 2 - Fabric energy Efficiency

Fabric energy Efficiency: 38.39

Credits awarded for ENE 2 = 7.2

ENE 7 - Low or Zero Carbon (LZC) Technologies

Reduction in CO2 Emissions

| | % | kg/m²/year | L |
|-----------------------------|---|------------|---|
| Standard Case CO2 emissions | | 35.98 | |
| Standard DER | | 17.76 | |
| Actual Case CO2 emissions | | 35.98 | |
| Actual DER | | 17.76 | |
| Reduction in CO2 emissions | 0 | | |

.

Credits awarded for ENE 7 = 0

Technologies eligible to contribute to achieving the requirements of this issue must produce energy from renewable sources and meet all other ancillary requirements as defined by Directive 2009/28/EC of the European Parliament and of the Council of 23 April 2009 on the promotion of the use of energy from renewable sources and amending and subsequently repealing Directives 2001/77/EC and 2003/30/EC.

The following requirements must also be met:

- Where not provided by accredited external renewables there must be a direct supply of energy produced to the dwelling under assessment.
- Where covered by the Microgeneration Certification Scheme (MCS), technologies under 50kWe or 300kWth must be certified.
- Combined Heat and Power (CHP) schemes above 50kWe must be certified under the CHPQA standard.

· All technologies must be accounted for by SAP.

CHP schemes fuelled by mains gas are eligible to contribute to performance against this issue. Where these schemes are above 50kWe they must be certified under the CHPOA. It is the responsibly of the Accredited OCDEA and Code Assessor to ensure all technologies use in the calculation are appropriate before awarding credits.



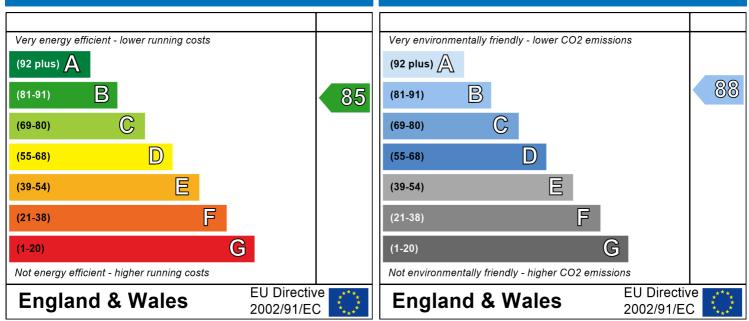
Dwelling type: Date of assessment: Produced by: Total floor area: Mid-terrace House 01 August 2019 Mitchel Armitage-Neiles 82.76 m²

Environmental Impact (CO₂) Rating

This is a Predicted Energy Assessment for a property which is not yet complete. It includes a predicted energy rating which might not represent the final energy rating of the property on completion. Once the property is completed, an Energy Performance Certificate is required providing information about the energy performance of the completed property.

Energy performance has been assessed using the SAP 2012 methodology and is rated in terms of the energy use per square metre of floor area, energy efficiency based on fuel costs and environmental impact based on carbon dioxide (CO2) emissions.

Energy Efficiency Rating



The energy efficiency rating is a measure of the overall efficiency of a home. The higher the rating the more energy efficient the home is and the lower the fuel bills are likely to be. The environmental impact rating is a measure of a home's impact on the environment in terms of carbon dioxide (CO2) emissions. The higher the rating the less impact it has on the environment.

SAP Input

Property Details: Plot 104 Dart [Mid] DCC3

| Address: Located in: Region: UPRN: Date of assessme Date of certificat Assessment type Transaction type Tenure type: Related party dis Thermal Mass Pa Water use <= 12 PCDF Version: | ent: :e: :: :: sclosure: arameter: | Engla South 01 Au 13 Jai New o New o Unkno No re Calcu | East England gust 2019 nuary 2020 dwelling design stag dwelling | ge | | | | |
|--|---|--|---|---|--|------------------------------------|--------------------------|---------------|
| Property description | 1: | | | | | | | |
| Dwelling type: Detachment: Year Completed: | | House Mid-te 2019 | e errace | | | | | |
| Floor Location: | | Floo | r area: | | | | | |
| Floor 0 Floor 1 | | 41.38 41.38 | | ç | Storey height 2.31 m 2.61 m | : | | |
| Living area: Front of dwelling fa | aces: | 14.96 North | m ² (fraction 0.18 West | 1) | | | | |
| Opening types: | | | | | | | | |
| Name: Door Front Rear Patio | Source: Manufacturer Manufacturer Manufacturer Manufacturer | 5 \ \ | Гуре: Solid Windows Windows Windows | low-E, En = low-E, En = | 0.2, hard coat 0.2, hard coat 0.2, hard coat 0.2, hard coat | Argon: Yes Yes Yes Yes | Fram PVC-L | |
| Name: Door Front Rear Patio | 16mm o 16mm o 16mm o | r more r more | Frame Facto 0.7 0.7 0.7 0.7 0.7 | 0.72 0.72 0.72 0.72 | U-value: 1.1 1.2 1.2 1.5 | Area: 2.05 4.76 3 5.22 | 1 1 1 1 | of Openings: |
| Name: Door Front Rear Patio | Type-Name | | Location: Walls Walls Walls Walls | Orient: North West North West South East South East | | Width: 0 0 0 0 | Heig 0 0 0 0 | |
| Overshading: Opaque Elements: | | Avera | ge or unknown | | | | | |
| Туре: (| Gross area: | Openings: | Net area: | U-value: | Ru value: | Curtain | wall | Kappa: |
| External Elements Walls External Roof Floor | 65.91 41.38 41.38 | 15.03 0 | 50.88 41.38 | 0.28 0.11 0.12 | 0 0 | False | wan. | 48 9 75 |
| <u>Internal Elements</u> Stud Ceiling | 137.01 41.38 | | | | | | | 9 9 |

SAP Input

| Floor Dorty Flomonto | 41.38 | | | | | 18 |
|--|----------------|--|--|---|--|----------|
| <u>Party Elements</u> Party Wall | 65.45 | | | | | 48 |
| Thermal bridges: | | | | | | |
| Thermal bridges: | | Length | Psi-value | values) | Y-Value = 0.0432 | |
| | | 9.7 6.23 20.1 18.19 9.16 9.16 15.06 4.62 9.08 18.16 | 0.236 0.01 0.005 0.089 -0.002 0.053 0.041 0.051 0.043 0.035 | E1 E3 E4 E5 E6 E10 E18 E16 P1 P4 | Steel lintel with perforated steel base plate Sill Jamb Ground floor (normal) Intermediate floor within a dwelling Eaves (insulation at ceiling level) Party wall between dwellings Corner (normal) Ground floor Roof (insulation at ceiling level) | |
| Ventilation: | | | | | | |
| Pressure test: Ventilation: Number of chimneys Number of open flue Number of fans: Number of passive s Number of sides she Pressure test: | es: stacks: | Yes (As desig Natural ventil 0 0 3 0 2 5.01 | ned) ation (extract fa | ans) | | |
| Main heating system: | : | | | | | |
| Main heating system | | Gas boilers an Fuel: mains g Info Source: I Database: (re Brand name: Model: LOGIC Model qualifie (Combi boiler Systems with Central heatir | as Boiler Database ev 454, product Ideal C COMBI er: ESP1 35) radiators ng pump : 2013 emperature: Deck: Yes | index C | 017929) Efficiency: Winter 87.3 % Summe | er: 90.5 |
| Main heating Control | | 2 | | | | |
| Main heating Contro | | Programmer, Control code: | room thermost 2106 | at and | TRVs | |
| Secondary heating sy | | | | | | |
| Secondary heating s Water heating: | | None | | | | |
| Water heating: | | From main he Water code: 9 Fuel :mains g No hot water Solar panel: F | 901 jas cylinder | | | |
| Others: | | р | | | | |
| Electricity tariff: In Smoke Control Ar | rea: | Standard Tari Unknown | iff | | | |

SAP Input

Conservatory: Low energy lights: Terrain type: EPC language: Wind turbine: Photovoltaics: Assess Zero Carbon Home: No conservatory 100% Low rise urban / suburban English No None No

| | | | | User D | etails: | | | | | | |
|--|--------------------------|-------------------------|----------|--------------------------------|-----------------|-------------|-------------------|-----------|-----------|-------------------------|------|
| Assessor Name: Software Name: | Mitchel Arr Stroma FS | nitage-Neile AP 2012 | es | | Strom Softwa | | | | | 0029948 on: 1.0.4.23 | |
| | | | Pr | operty / | Address | Plot 10 | 4 Dart [N | /lid] DC(| 23 | | |
| Address : | | | | | | | | | | | |
| 1. Overall dwelling dime | ensions: | | | | | | | | | | |
| | | | | Area | a(m²) | | Av. Hei | ight(m) | | Volume(m ³) | |
| Ground floor | | | | 4 | 1.38 | (1a) x | 2. | .31 | (2a) = | 95.59 | (3a) |
| First floor | | | | 4 | 1.38 | (1b) x | 2. | .61 | (2b) = | 108 | (3b) |
| Total floor area TFA = (1 | a)+(1b)+(1c)+ | (1d)+(1e)+ | (1n) |) 8 | 2.76 | (4) | | | - | | |
| Dwelling volume | | | | | | (3a)+(3b) |)+(3c)+(3d |)+(3e)+ | .(3n) = | 203.59 | (5) |
| 2. Ventilation rate: | | | | | | | | | | | |
| | main heating | secor heati | | / | other | | total | | | m ³ per hour | |
| Number of chimneys | 0 | + 0 | - | + | 0 |] = [| 0 | X 4 | 40 = | 0 | (6a) |
| Number of open flues | 0 | + 0 |) | + | 0 |] = [| 0 | × 2 | 20 = | 0 | (6b) |
| Number of intermittent fa | ns | | | | | | 3 | x ^ | 0 = | 30 | (7a) |
| Number of passive vents | | | | | | Γ | 0 | × ^ | 0 = | 0 | (7b) |
| Number of flueless gas fi | res | | | | | Γ | 0 | x 4 | 40 = | 0 | (7c) |
| | | | | | | | | | A in ak | | _ |
| Infiltration due to chimne | | | b) (7 |),(7 h),([*] | 70) - | _ | | | | hanges per hou | 1 |
| Infiltration due to chimne | | | | | | continue fr | 30 om (9) to (| | ÷ (5) = | 0.15 | (8) |
| Number of storeys in the | | | 00000 | to (<i>11)</i> , c | | | | 10) | | 0 | (9) |
| Additional infiltration | 9.(| , | | | | | | [(9)- | -1]x0.1 = | 0 | (10) |
| Structural infiltration: 0 | .25 for steel or | r timber fram | e or | 0.35 for | masonr | y constr | uction | | | 0 | (11) |
| if both types of wall are p | | | ing to | the greate | er wall are | a (after | | | | | 1 |
| deducting areas of openin If suspended wooden f | 0 // 1 | | or 0.′ | 1 (seale | d), else | enter 0 | | | | 0 | (12) |
| If no draught lobby, en | | · , | | , | ,, | | | | | 0 | (13) |
| Percentage of windows | s and doors dr | aught strippe | əd | | | | | | | 0 | (14) |
| Window infiltration | | | | | 0.25 - [0.2 | x (14) ÷ 1 | = [00 | | | 0 | (15) |
| Infiltration rate | | | | | (8) + (10) | + (11) + (1 | 2) + (13) + | + (15) = | | 0 | (16) |
| Air permeability value, | q50, expresse | ed in cubic m | etres | s per ho | our per so | quare m | etre of e | nvelope | area | 5.01000022888184 | (17) |
| If based on air permeabil | ity value, then | (18) = [(17) ÷ 2 | 20]+(8 |), otherwi | se (18) = (| 16) | | | | 0.4 | (18) |
| Air permeability value applie | | on test has beel | n done | e or a deg | ree air pe | rmeability | is being us | sed | | | |
| Number of sides sheltere | ed | | | | (20) – 1 | [0 075 v (1 | 0)1 | | | 2 | (19) |
| Shelter factor | ing chalter for | 4.5.4 | | | (20) = 1 - | | 9)] = | | | 0.85 | (20) |
| Infiltration rate incorporat | • | | | | (21) = (18) | , | | | | 0.34 | (21) |
| Infiltration rate modified f | Mar Apr | · · | un | Jul | Δυσ | Sep | Oct | Nov | Dec | 1 | |
| | | · · · | | Jui | Aug | Jeh | | | Dec |] | |
| Monthly average wind sp | | <u> </u> | <u> </u> | 2.0 | 0.7 | Α | 4.2 | A E | 4 7 | 1 | |
| (22)m= 5.1 5 | 4.9 4.4 | 4.3 3. | ° | 3.8 | 3.7 | 4 | 4.3 | 4.5 | 4.7 | | |

| Wind F | actor (2 | 22a)m = | (22)m ÷ | 4 | | | | | | | | | |
|---------|------------|----------------------------|-----------|------------|-------------------------------|----------|------------|-----------------------|-------------|-------------|-------------|-------------|---------------|
| (22a)m= | 1.27 | 1.25 | 1.23 | 1.1 | 1.08 | 0.95 | 0.95 | 0.92 | 1 | 1.08 | 1.12 | 1.18 | |
| Adjuste | ed infiltr | ation rat | e (allow | ing for sl | nelter an | d wind s | speed) = | (21a) x | (22a)m | | | | |
| | 0.43 | 0.42 | 0.41 | 0.37 | 0.36 | 0.32 | 0.32 | 0.31 | 0.34 | 0.36 | 0.38 | 0.4 | |
| | | ctive air | - | rate for t | he appli | cable ca | se | | | | 1 | ں ح | |
| | | al ventila | | | (00) | | | | |) (00-) | | Ļ | 0 (23a) |
| | | eat pump | 0 11 | | , (| , | • | ,, . | , | o) = (23a) | | Ļ | 0 (23b) |
| | | h heat reco | | | • | | | | | | | | 0 (23c) |
| | | 1 | I | i | · · · · · · | 1 | <u> </u> | 1 | ŕ | <u> </u> | <u> </u> | 1 – (23c) · | - |
| (24a)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | (24a) |
| | | ed mecha | | 1 | · · · · · · | | | 1 | ŕ | 1 | <u> </u> | | (24b) |
| (24b)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | (240) |
| | | nouse ex n < 0.5 × | | | | | | | | 5 x (23) | n) | | |
| (24c)m= | 0 | | | | $\frac{0}{0} = \frac{201}{2}$ | | | $\frac{0}{0} = (221)$ | | | 0 | 0 | (24c) |
| | | ventilatio | _ | | | - | - | - | | Ů | Ů | <u> </u> | |
| , | | n = 1, the | | | • | • | | | | 0.5] | | | |
| (24d)m= | 0.59 | 0.59 | 0.59 | 0.57 | 0.57 | 0.55 | 0.55 | 0.55 | 0.56 | 0.57 | 0.57 | 0.58 | (24d) |
| Effe | ctive air | change | rate - er | nter (24a | u) or (24t |) or (24 | c) or (24 | d) in bo | x (25) | | 4 | | |
| (25)m= | 0.59 | 0.59 | 0.59 | 0.57 | 0.57 | 0.55 | 0.55 | 0.55 | 0.56 | 0.57 | 0.57 | 0.58 | (25) |
| 3 He | at losse | s and he | at loss i | naramet | ≏r. | | | - | - | - | - | | |
| ELEN | | Gros | | Openir | | Net Ar | ea | U-val | ue | ΑXU | | k-value | AXk |
| | | area | | n | - | A ,r | | W/m2 | | (W/ | | kJ/m²•K | |
| Doors | | | | | | 2.05 | x | 1.1 | = | 2.255 | | | (26) |
| Window | ws Type | e 1 | | | | 4.76 | x1 | /[1/(1.2)+ | 0.04] = | 5.45 | | | (27) |
| Window | ws Type | e 2 | | | | 3 | x1 | /[1/(1.2)+ | 0.04] = | 3.44 | | | (27) |
| Window | ws Type | e 3 | | | | 5.22 | | /[1/(1.5)+ | 0.04] = | 7.39 | | | (27) |
| Floor | | | | | | 41.38 | 3 X | 0.12 | | 4.9656 | | 75 | 3103.5 (28) |
| Walls | | 65.9 | 91 | 15.0 | 3 | 50.88 | | 0.28 | | 14.25 | | 48 | 2442.24 (29) |
| Roof | | 41.3 | | 0 | | 41.38 | | 0.11 | | 4.55 | | 9 | 372.42 (30) |
| | rea of e | elements | | | | 148.6 | | 0.11 | | 4.00 | [| 5 | (31) |
| Party v | | | , | | | | | | | 0 | r | 40 | |
| • | l wall * | ÷ | | | | 65.45 | | 0 | = | 0 | | 48 | |
| | | | | | | 137.0 | | | | | L | 9 | 1233.09 (32c) |
| Interna | | | | | | 41.38 | | | | | l | 18 | 744.84 (32d) |
| | l ceiling | | | <i>.</i> | | 41.38 | | | | | | 9 | 372.42 (32e) |
| | | l roof winde as on both | | | | | ated using | g formula 1 | /[(1/U-valu | ue)+0.04] a | as given in | paragraph | 3.2 |

| Fabric heat loss, W/K = S (A x U) | (26)(30) + (32) = | 42.29 | (33) |
|--|---------------------------------|----------|------|
| Heat capacity $Cm = S(A \times k)$ | ((28)(30) + (32) + (32a)(32e) = | 11410.11 | (34) |
| Thermal mass parameter (TMP = $Cm \div TFA$) in kJ/m ² K | = (34) ÷ (4) = | 137.87 | (35) |

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f

| Thermal bridges : S (L x Y) calculated using Appendix K 6.42 if details of thermal bridging are not known (36) = 0.05 x (31) (33) + (36) = 48.71 Total fabric heat loss (33) + (36) = 48.71 Ventilation heat loss calculated monthly (38)m = 0.33 × (25)m × (5) (38)m = 0.33 × (25)m × (5) (38)m = 39.84 39.59 39.36 38.24 38.03 37.06 36.88 37.43 38.03 38.45 38.9 Heat transfer coefficient, W/K (39)m = (37) + (38)m (39)m = (37) + (38)m (39)m = (37) + (38)m (40)m = (37) + (38)m (40)m = (37) + (38)m (40)m = (39)m + (4) (41)m = 31 28 31 30 31 30 31 30 31 31 30 31 31 30 31 (41)m = 31 28 31 30 31 30 31 31 30 31 31 30 31 (41)m = 31 28 31 30 31 30 31 31 30 31 31 30 31 (41)m = | $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | | |
|---|---|--|--|--|---|
| Total fabric heat loss (33) + (36) = 48.71 Ventilation heat loss calculated monthly (38)m = 0.33 × (25)m × (5) (38)m = 0.33 × (25)m × (5) (38)m = 39.84 39.59 39.36 38.24 38.03 37.06 36.88 37.43 38.03 38.45 38.9 Heat transfer coefficient, W/K (39)m = (37) + (38)m (39)m = (37) + (38)m 39.84 38.07 86.95 86.74 85.77 85.59 86.14 86.74 87.6 Heat transfer coefficient, W/K (39)m = (37) + (38)m $400m$ = (39)m = (37) + (38)m $400m$ $490m$ | eat loss (33) + (36) = (48.71) (37) eat loss calculated monthly (38)m = 0.33 × (25)m × (5) (38)m = 0.33 × (25)m × (5) (38)m = 0.33 × (25)m × (5) Feb Mar Apr May Jun Jul Aug Sep Oct Nov Dec 39.59 39.36 38.24 38.03 37.06 36.88 37.43 38.03 38.45 38.9 (38) coefficient, W/K (39)m = (37) + (38)m (39)m = (37) + (38)m (39) Average = Sum(39)_{1-12} / 12= 86.95 (39) rameter (HLP), W/m ² K (40)m = (39)m ÷ (4) (40) 1.07 1.06 1.05 1.04 1.04 1.03 1.04 1.05 1.06 ays in month (Table 1a) Average = Sum(40)_{1-12} / 12= (40) 28 31 30 31 30 31 30 31 30 31 (41) | | | | |
| Ventilation heat loss calculated monthly (38)m = 0.33 × (25)m × (5) Jan Feb Mar Apr May Jun Jul Aug Sep Oct Nov Dec (38)m = 39.84 39.59 39.36 38.24 38.03 37.06 36.88 37.43 38.03 38.45 38.9 Heat transfer coefficient, W/K (39)m = (37) + (38)m (39)m = (37) + (38)m Average = Sum(39)2 /12= 86.95 Heat loss parameter (HLP), W/m2K (40)m = (39)m ÷ (4) Average = Sum(39)2 /12= 86.95 Heat loss parameter (HLP), W/m2K (40)m = (39)m ÷ (4) Average = Sum(40)2 /12= 1.05 Number of days in month (Table 1a) Average = Sum(40)2 /12= 1.05 1.05 (41)m = 31 28 31 30 31 30 31 30 31 4. Water heating energy requirement: KWh/year: Assumed occupancy, N 2.51 2.51 | total with the second | | | | |
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| (44)m= 103.28 99.52 95.76 92.01 88.25 84.5 88.25 92.01 95.76 99.52 103.28 Total = Sum(44) 100 x Vd,m x nm x DTm / 3600 kWh/month (see Tables 1b, 1c, 1d) Total = Sum(44) 1126.65 Energy content of hot water used - calculated monthly = 4.190 x Vd,m x nm x DTm / 3600 kWh/month (see Tables 1b, 1c, 1d) (45)m= 153.16 133.95 138.22 120.51 115.63 99.78 92.46 106.1 107.37 125.13 136.59 148.32 Total = Sum(45) 148.32 Total = Sum(45) 1477.21 If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61) (46)m= 22.97 20.09 20.73 18.08 17.34 14.97 13.87 15.92 16.11 18.77 20.49 22.25 Water storage loss: Storage volume (litres) including any solar or WWHRS storage within same vessel 0 If community heating and no tank in dwelling, enter 110 litres in (47) 0 Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in | The set of the | | | | |
| (44)m= 103.28 99.52 95.76 92.01 88.25 84.5 88.25 92.01 95.76 99.52 103.28 Total = Sum(44):=:= 1126.65 Energy content of hot water used - calculated monthly = 4.190 x Vd,m x nm x DTm / 3600 kWh/month (see Tables 1b, 1c, 1d) (45)m= 153.16 133.95 138.22 120.51 115.63 99.78 92.46 106.1 107.37 125.13 136.59 148.32 Total = Sum(45):=:= 1477.21 If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61) (46)m= 22.97 20.09 20.73 18.08 17.34 14.97 13.87 15.92 16.11 18.77 20.49 22.25 Water storage loss: Storage volume (litres) including any solar or WWHRS storage within same vessel 0 If manufacturer's declared loss factor is known (kWh/day): 0 O O Item storage loss: a) If manufacturer's declared loss factor is known (kWh/day): | Total = Sum(44): | | | | |
| (44)m= 103.28 99.52 95.76 92.01 88.25 84.5 88.25 92.01 95.76 99.52 103.28 Total = Sum(44) 100 x Vd,m x nm x DTm / 3600 kWh/month (see Tables 1b, 1c, 1d) Total = Sum(44) 1126.65 Energy content of hot water used - calculated monthly = 4.190 x Vd,m x nm x DTm / 3600 kWh/month (see Tables 1b, 1c, 1d) (45)m= 153.16 133.95 138.22 120.51 115.63 99.78 92.46 106.1 107.37 125.13 136.59 148.32 Total = Sum(45) 148.32 Total = Sum(45) 1477.21 If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61) (46)m= 22.97 20.09 20.73 18.08 17.34 14.97 13.87 15.92 16.11 18.77 20.49 22.25 Water storage loss: Storage volume (litres) including any solar or WWHRS storage within same vessel 0 If community heating and no tank in dwelling, enter 110 litres in (47) 0 Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in | age hot water usage in litres per day Vd,average = $(25 \times N) + 36$ (43)ual average hot water usage by 5% if the dwelling is designed to achieve a water use target of(43)September 2010(43)93.89(43)(43)Feb Mar Apr May Jun Jul Aug Sep Oct Nov Decin litres per day for each month Vd,m = factor from Table 1c x (43)Total = Sum(44) | | | | |

| | | m water (54) in (5 | - | e, kWh/y | ear | | | (47) x (51) |) x (52) x (| 53) = | | 0 | | (54) |
|----------|-----------|------------------------|-----------|---|------------|-------------|-----------------|--------------|---------------|----------------|-------------|-------------|---------------|------|
| | . , | . , . | | for oach | month | | | ((56)m - (| 55) v (41) | ~ | | 0 | | (55) |
| | | i | i | for each | | | | | 55) × (41)ı | | 1 | | I | (50) |
| (56)m= | | 0 dedicate | | 0 | 0 | 0 | 0 | 0 | 0 | 0 m whore (| 0 | 0 | iu I I | (56) |
| n cynnae | ercontain | | | nage, (57) | m = (oc)m | x [(50) – (| (ס – [(יוח ד | 0), eise (5 | /)ffi = (56) | m where (| | m Append | | |
| (57)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | (57) |
| Primar | y circuit | loss (ar | nual) fro | om Table | e 3 | | | | | | | 0 | | (58) |
| | • | | | | | , | (58) ÷ 36 | . , | | | | | | |
| | | 1 | rom Tab | i | I | · · · · · · | | <u> </u> | cylinde | | <u> </u> | 1 | I | |
| (59)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | (59) |
| Combi | loss ca | lculated | for each | month | (61)m = | (60) ÷ 30 | 65 × (41) |)m | | | | | | |
| (61)m= | 14.12 | 12.75 | 14.07 | 13.58 | 14 | 13.52 | 13.94 | 13.98 | 13.55 | 14.04 | 13.64 | 14.11 | | (61) |
| Total h | neat req | uired for | water h | eating ca | alculated | for eac | h month | (62)m = | 0.85 × (| (45)m + | (46)m + | (57)m + | (59)m + (61)m | |
| (62)m= | 167.28 | 146.7 | 152.3 | 134.09 | 129.63 | 113.3 | 106.4 | 120.08 | 120.92 | 139.17 | 150.22 | 162.44 | | (62) |
| Solar DI | -IW input | calculated | using App | endix G o | r Appendix | H (negati | ve quantity | /) (enter '0 | ' if no sola | r contribut | ion to wate | er heating) | | |
| (add a | dditiona | l lines if | FGHRS | and/or \ | NWHRS | applies | , see Ap | pendix (| G) | | | | | |
| (63)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | (63) |
| Output | t from w | ater hea | ter | | | - | | - | - | | | | | |
| (64)m= | 167.28 | 146.7 | 152.3 | 134.09 | 129.63 | 113.3 | 106.4 | 120.08 | 120.92 | 139.17 | 150.22 | 162.44 | | |
| | | | | • | | | • | Outp | but from wa | ater heate | r (annual)₁ | 12 | 1642.52 | (64) |
| Heat g | ains fro | m water | heating | , kWh/m | onth 0.2 | 5 ´ [0.85 | × (45)m | ı + (61)m | n] + 0.8 x | (46)m | + (57)m | + (59)m |] | |
| (65)m= | 54.46 | 47.72 | 49.48 | 43.46 | 41.95 | 36.56 | 34.23 | 38.77 | 39.09 | 45.12 | 48.82 | 52.85 | - | (65) |
| inclu | ude (57) | m in calo | culation | • of (65)m | only if c | vlinder i | s in the o | dwelling | or hot w | ater is fr | om com | munity h | eating | |
| | . , | | | 5 and 5a | - | , | | 0 | | | | , | 0 | |
| | | | | | /• | | | | | | | | | |
| Melab | Jan | <u>s (Table</u> Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | |
| (66)m= | | 150.79 | | | | | | 150.79 | | | 150.79 | | | (66) |
| | | | | 1 | | | r L9a), a | | | | | | | |
| (67)m= | 52.55 | 46.68 | 37.96 | 28.74 | 21.48 | 18.14 | 19.6 | 25.47 | 34.19 | 43.41 | 50.67 | 54.01 | | (67) |
| | | | | | | | | | see Tal | | 00.01 | 01.01 | | (-) |
| (68)m= | 335.99 | 339.47 | 330.69 | 311.98 | 288.37 | 266.18 | 251.36 | 247.87 | 256.66 | 275.36 | 298.97 | 321.16 | | (68) |
| | | | | | | | | | | | 290.97 | 521.10 | | (00) |
| | <u> </u> | (caicula 52.59 | 52.59 | 52.59 | L, equa | 52.59 | or L15a) | | e Table | | 50.50 | 52.59 | I | (69) |
| (69)m= | 52.59 | | | | 52.59 | 52.59 | 52.59 | 52.59 | 52.59 | 52.59 | 52.59 | 52.59 | | (09) |
| | r | ns gains | r` | <u>, </u> | | | | | | | | | I | (70) |
| (70)m= | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | | (70) |
| | | · · | | tive valu | <u> </u> | · · | 1 | i | i | | 1 | i | I | |
| | | -100.53 | -100.53 | -100.53 | -100.53 | -100.53 | -100.53 | -100.53 | -100.53 | -100.53 | -100.53 | -100.53 | | (71) |
| Water | | gains (T | able 5) | | | | | | | | | | I | |
| (72)m= | 73.19 | 71.02 | 66.5 | 60.37 | 56.38 | 50.77 | 46.01 | 52.12 | 54.29 | 60.64 | 67.81 | 71.03 | | (72) |
| Total i | nternal | gains = | | | | (66) |)m + (67)m | n + (68)m - | + (69)m + (| (70)m + (7 | 1)m + (72) | m | | |
| (73)m= | 567.59 | 563.03 | 541.01 | 506.94 | 472.09 | 440.95 | 422.82 | 431.31 | 450.99 | 485.27 | 523.31 | 552.06 | | (73) |
| 6. So | lar gains | S: | | | | | | | | | | | | |

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

| Orientation: | Access Factor Table 6d | - | Area m² | | Flux Table 6a | | g_ Table 6b | | FF Table 6c | | Gains (W) | |
|----------------|---------------------------|---|------------|---|------------------|---|----------------|---|----------------|---|--------------|------|
| Southeast 0.9x | 0.77 | x | 3 | x | 36.79 | × | 0.72 | x | 0.7 | = | 38.55 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | × | 36.79 | x | 0.72 | x | 0.7 | = | 67.08 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | x | 62.67 | x | 0.72 | x | 0.7 | = | 65.67 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | × | 62.67 | x | 0.72 | x | 0.7 | = | 114.27 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | x | 85.75 | x | 0.72 | x | 0.7 | = | 89.85 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | × | 85.75 | x | 0.72 | x | 0.7 | = | 156.34 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | × | 106.25 | x | 0.72 | x | 0.7 | = | 111.33 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | x | 106.25 | x | 0.72 | x | 0.7 | = | 193.72 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | × | 119.01 | × | 0.72 | x | 0.7 | = | 124.7 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | × | 119.01 | x | 0.72 | x | 0.7 | = | 216.98 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | × | 118.15 | × | 0.72 | x | 0.7 | = | 123.8 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | × | 118.15 | x | 0.72 | x | 0.7 | = | 215.41 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | × | 113.91 | x | 0.72 | x | 0.7 | = | 119.36 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | × | 113.91 | × | 0.72 | x | 0.7 | = | 207.68 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | × | 104.39 | x | 0.72 | x | 0.7 | = | 109.38 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | x | 104.39 | x | 0.72 | x | 0.7 | = | 190.32 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | × | 92.85 | × | 0.72 | x | 0.7 | = | 97.29 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | × | 92.85 | × | 0.72 | x | 0.7 | = | 169.29 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | × | 69.27 | x | 0.72 | x | 0.7 | = | 72.58 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | × | 69.27 | × | 0.72 | x | 0.7 | = | 126.29 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | × | 44.07 | x | 0.72 | x | 0.7 | = | 46.18 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | × | 44.07 | × | 0.72 | x | 0.7 | = | 80.35 | (77) |
| Southeast 0.9x | 0.77 | x | 3 | × | 31.49 | × | 0.72 | x | 0.7 | = | 32.99 | (77) |
| Southeast 0.9x | 0.77 | x | 5.22 | × | 31.49 | × | 0.72 | x | 0.7 | = | 57.41 | (77) |
| Northwest 0.9x | 0.77 | x | 4.76 | × | 11.28 | x | 0.72 | x | 0.7 | = | 18.76 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | × | 22.97 | × | 0.72 | x | 0.7 | = | 38.18 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | × | 41.38 | × | 0.72 | x | 0.7 | = | 68.79 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | × | 67.96 | x | 0.72 | x | 0.7 | = | 112.98 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | × | 91.35 | × | 0.72 | x | 0.7 | = | 151.87 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | x | 97.38 | x | 0.72 | x | 0.7 | = | 161.91 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | x | 91.1 | x | 0.72 | x | 0.7 | = | 151.46 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | × | 72.63 | × | 0.72 | x | 0.7 | = | 120.74 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | × | 50.42 | x | 0.72 | x | 0.7 | = | 83.83 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | × | 28.07 | × | 0.72 | x | 0.7 | = | 46.66 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | × | 14.2 | × | 0.72 | x | 0.7 | = | 23.6 | (81) |
| Northwest 0.9x | 0.77 | x | 4.76 | × | 9.21 | x | 0.72 | x | 0.7 | = | 15.32 | (81) |

| Solar g | ains in | watts, ca | alculated | for eac | h month | | | (83)m = S | um(74)m . | (82)m | | _ | _ | |
|---------|-----------|-----------|-----------|---------|-----------|---------|---------|-----------|-----------|--------|--------|--------|------|----|
| (83)m= | 124.39 | 218.12 | 314.99 | 418.03 | 493.55 | 501.12 | 478.49 | 420.45 | 350.41 | 245.53 | 150.13 | 105.72 | (83) | ;) |
| Total g | ains – ii | nternal a | ind solar | (84)m = | = (73)m - | + (83)m | , watts | | | | | | | |
| (84)m= | 691.98 | 781.15 | 856 | 924.97 | 965.64 | 942.06 | 901.31 | 851.77 | 801.4 | 730.8 | 673.44 | 657.78 | (84 |) |

| 7. Me | an inter | nal temp | perature | (heating | season |) | | | | | | | | |
|---------|-----------|-----------|----------------------|------------|---------------|------------|--------------|------------|--------------|-------------|--------------|------------|---------|-------|
| | | | | | | | from Tal | ole 9, Th | 1 (°C) | | | [| 21 | (85) |
| Utilisa | ation fac | tor for g | ains for | living are | ea, h1,m | (see Ta | ble 9a) | | | | | I | | |
| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | |
| (86)m= | 0.96 | 0.94 | 0.9 | 0.82 | 0.7 | 0.54 | 0.41 | 0.44 | 0.65 | 0.85 | 0.94 | 0.96 | | (86) |
| Mean | interna | l temper | ature in | living are | ea T1 (fo | ollow ste | ps 3 to 7 | 7 in Tabl | e 9c) | | | | | |
| (87)m= | 19.53 | 19.76 | 20.08 | 20.47 | 20.76 | 20.93 | 20.98 | 20.97 | 20.87 | 20.49 | 19.95 | 19.49 | | (87) |
| Temp | erature | during h | neating p | eriods ir | n rest of | dwelling | from Ta | able 9, T | h2 (°C) | | | | | |
| (88)m= | 20.03 | 20.03 | 20.03 | 20.04 | 20.04 | 20.05 | 20.05 | 20.05 | 20.05 | 20.04 | 20.04 | 20.03 | | (88) |
| Utilisa | ation fac | tor for g | ains for | rest of d | welling, | h2,m (se | e Table | 9a) | | | | | | |
| (89)m= | 0.95 | 0.93 | 0.88 | 0.79 | 0.65 | 0.47 | 0.32 | 0.36 | 0.58 | 0.82 | 0.92 | 0.96 | | (89) |
| Mean | interna | l temper | ature in | the rest | of dwelli | ng T2 (f | ollow ste | eps 3 to | 7 in Tabl | le 9c) | | | | |
| (90)m= | 18.7 | 18.92 | 19.24 | 19.61 | 19.87 | 20.01 | 20.05 | 20.04 | 19.97 | 19.64 | 19.12 | 18.67 | | (90) |
| | | | | | | | • | | . 1 | fLA = Livin | ig area ÷ (4 | 4) = | 0.18 | (91) |
| Mean | interna | l temper | ature (fo | or the wh | ole dwe | lling) = f | LA x T1 | + (1 – fL | .A) × T2 | | | | | |
| (92)m= | 18.85 | 19.08 | 19.39 | 19.77 | 20.04 | 20.18 | 20.21 | 20.21 | , 20.13 | 19.79 | 19.27 | 18.82 | | (92) |
| Apply | adjustr | nent to t | he mear | interna | l temper | ature fro | m Table | 4e, whe | ere appro | opriate | 1 | | | |
| (93)m= | 18.7 | 18.93 | 19.24 | 19.62 | 19.89 | 20.03 | 20.06 | 20.06 | 19.98 | 19.64 | 19.12 | 18.67 | | (93) |
| 8. Sp | ace hea | ting requ | uirement | | | | | | - | | | | | |
| | | | | • | | ned at st | ep 11 of | Table 9 | b, so tha | ıt Ti,m=(| 76)m an | d re-calc | ulate | |
| the ut | | factor fo | <u> </u> | | 1 | | | | | | | | | |
| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | |
| (94)m= | 0.94 | tor for g | 0.86 | 0.78 | 0.64 | 0.47 | 0.32 | 0.36 | 0.58 | 0.8 | 0.91 | 0.95 | | (94) |
| | | hmGm | | | | 0.47 | 0.52 | 0.50 | 0.00 | 0.0 | 0.31 | 0.95 | | (01) |
| (95)m= | 649.13 | 711.57 | , VV – (9. 739.83 | 718.88 | 622.23 | 444.21 | 292.84 | 307.14 | 462.53 | 585.52 | 611.78 | 622.03 | | (95) |
| | | age exte | | | | | | | 102.00 | 000102 | | 012.00 | | |
| (96)m= | 4.3 | 4.9 | 6.5 | 8.9 | 11.7 | 14.6 | 16.6 | 16.4 | 14.1 | 10.6 | 7.1 | 4.2 | | (96) |
| Heat | loss rate | e for me | an interr | al tempe | i erature, | Lm , W = | i =[(39)m | r [(93)m | i – (96)m | 1 | | <u> </u> | | |
| (97)m= | r | 1238.47 | 1 | 931.99 | 710.01 | 465.65 | 297.13 | 313.39 | 506.42 | 784.5 | 1048 | 1267.27 | | (97) |
| Space | e heatin | g require | ement fo | r each n | nonth, k | Nh/mon | th = 0.02 | 24 x [(97 |)m – (95 |)m] x (4 | 1)m | | | |
| (98)m= | 465.93 | 354.08 | 284.55 | 153.44 | 65.3 | 0 | 0 | 0 | 0 | 148.04 | 314.08 | 480.06 | | |
| | | | | | | | | Tota | l per year | (kWh/yea | r) = Sum(9 | 8)15,912 = | 2265.49 | (98) |
| Space | e heatin | g require | ement in | kWh/m² | ²/year | | | | | | | | 27.37 | (99) |
| 9a. En | ergy rec | quiremer | nts – Ind | ividual h | eating s | ystems i | ncluding | j micro-C | CHP) | | | • | | |
| - | e heatir | - | | | | | | | | | | | | |
| Fracti | ion of sp | bace hea | at from s | econdar | y/supple | mentary | y system | | | | | | 0 | (201) |
| Fracti | ion of sp | bace hea | at from m | nain syst | em(s) | | | (202) = 1 | – (201) = | | | | 1 | (202) |
| Fracti | ion of to | tal heati | ng from | main sys | stem 1 | | | (204) = (2 | 02) × [1 – | (203)] = | | | 1 | (204) |
| Efficie | ency of I | main spa | ace heat | ing syste | em 1 | | | | | | | | 90.5 | (206) |
| Efficie | ency of a | seconda | ry/suppl | ementar | y heatin | g systen | n, % | | | | | ĺ | 0 | (208) |
| | | | | | | | | | | | | • | | _ |

| 1 | | | i | | | | | · · · · · · | · · · · · · | | | | • | |
|----------|----------------------------|---------------------|---------------------|-----------|------------------|----------|----------|-------------|-------------|-----------------------|--------------------------|----------------------|-----------|------------|
| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | kWh/yea | ar |
| Space | e heating 465.93 | g require 354.08 | ement (c 284.55 | alculate | d above) 65.3 | 0 | 0 | 0 | 0 | 148.04 | 314.08 | 480.06 | 1 | |
| (011) | | | | | | 0 | 0 | 0 | 0 | 140.04 | 314.00 | 400.00 | | (011) |
| (211)m | $1 = \{[(98) \\ 514.84 \}$ | m x (20) 391.25 | 4)] } X 1 314.42 | 00 ÷ (20 | 72.16 | 0 | 0 | 0 | 0 | 163.58 | 347.05 | 530.45 | 1 | (211) |
| | | | _ | | | | | | | ar) =Sum(2 | | | 2503.3 | (211) |
| Space | e heating | g fuel (s | econdar | y), kWh/ | month | | | | | | | | | 1 |
| |)m x (20 | 1)]}x 1 | 00 ÷ (20 |)8) | | | | | | | | | 1 | |
| (215)m= | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | ٦ |
| Matan | h a a tim a | | | | | | | Tota | ii (kwn/yea | ar) =Sum(2 | 215) _{15,10} 12 | = | 0 | (215) |
| | heating from wa | | ter (calc | ulated a | bove) | | | | | | | | | |
| •p | 167.28 | 146.7 | 152.3 | 134.09 | 129.63 | 113.3 | 106.4 | 120.08 | 120.92 | 139.17 | 150.22 | 162.44 | | |
| Efficier | ncy of wa | ater hea | iter | | | | | | | | | | 87.3 | (216) |
| (217)m= | 89.63 | 89.54 | 89.36 | 88.98 | 88.35 | 87.3 | 87.3 | 87.3 | 87.3 | 88.92 | 89.44 | 89.67 | | (217) |
| | r water I = (64)r | • | | | | | | | | | | | | |
| (219)m= | | 163.84 | 170.44 | 150.69 | 146.73 | 129.78 | 121.88 | 137.55 | 138.51 | 156.51 | 167.96 | 181.15 |] | |
| | | | | • | | | | Tota | l = Sum(2 | 19a) ₁₁₂ = | | | 1851.67 | (219) |
| | I totals | | | | | | | | | k | Wh/year | | kWh/year | - |
| Space | heating | fuel use | ed, main | system | 1 | | | | | | | | 2503.3 | |
| Water | heating | fuel use | d | | | | | | | | | | 1851.67 | |
| Electric | city for p | umps, f | ans and | electric | keep-ho | t | | | | | | | | |
| centra | al heatin | g pump | : | | | | | | | | | 30 |] | (230c) |
| boiler | with a fa | an-assis | sted flue | | | | | | | | | 45 | | (230e) |
| Total e | lectricity | for the | above, l | kWh/yea | r | | | sum | of (230a). | (230g) = | | | 75 | (231) |
| Electric | city for lig | ghting | | | | | | | | | | | 371.24 | (232) |
| 10a. F | - uel cos | ts - indiv | /idual he | eating sy | stems: | | | | | | | | | |
| | | | | | | Fu | el | | | Fuel P | rice | | Fuel Cost | |
| | | | | | | | /h/year | | | (Table | | | £/year | |
| Space | heating | - main s | system 1 | l | | (21 | 1) x | | | 3.4 | 8 | x 0.01 = | 87.11 | (240) |
| Space | heating | - main s | system 2 | 2 | | (21: | 3) x | | | 0 | | x 0.01 = | 0 | (241) |
| Space | heating | - secon | dary | | | (21 | 5) x | | | 13. | 19 | x 0.01 = | 0 | (242) |
| Water | heating | cost (otl | her fuel) | | | (21 | 9) | | | 3.4 | 8 | x 0.01 = | 64.44 | (247) |
| Pumps | s, fans ai | nd elect | ric keep | -hot | | (23 | 1) | | | 13. | 19 | x 0.01 = | 9.89 | _ (249) |
| | | | | | 230a) se | eparatel | / as app | licable a | nd apply | | | dina to ⁻ | Table 12a |], , |
| | for light | | - (| | | (23 | | | | 13. | | x 0.01 = | 48.97 | (250) |
| Additio | nal stan | ding cha | arges (T | able 12) | | | | | | | | | 120 | (251) |
| Appen | dix Q ite | ms: rep | eat lines | s (253) a | nd (254) | as need | ded | | | | | | | |
| | energ | • | | () 0 | . , | | 50)(254) | = | | | | | 330.41 | (255) |

| 11a. SAP rating - individual heating syste | ems | | |
|--|---------------------------------|--------------------------------------|---------------------------------|
| Energy cost deflator (Table 12) | | | 0.42 (256) |
| Energy cost factor (ECF) | (255) x (256)] ÷ [(4) + 45.0] = | | 1.09 (257) |
| SAP rating (Section 12) | | | 84.85 (258) |
| 12a. CO2 emissions – Individual heating | systems including micro-CHP | | |
| | Energy kWh/year | Emission factor kg CO2/kWh | Emissions kg CO2/year |
| Space heating (main system 1) | (211) x | 0.216 = | 540.71 (261) |
| Space heating (secondary) | (215) x | 0.519 = | 0 (263) |
| Water heating | (219) x | 0.216 = | 399.96 (264) |
| Space and water heating | (261) + (262) + (263) + (2 | 264) = | 940.67 (265) |
| Electricity for pumps, fans and electric kee | ep-hot (231) x | 0.519 = | 38.93 (267) |
| Electricity for lighting | (232) x | 0.519 = | 192.67 (268) |
| Total CO2, kg/year | | sum of (265)(271) = | 1172.27 (272) |
| CO2 emissions per m ² | | (272) ÷ (4) = | 14.16 (273) |
| EI rating (section 14) | | | 88 (274) |
| 13a. Primary Energy | | | |
| | Energy kWh/year | Primary factor | P. Energy kWh/year |
| Space heating (main system 1) | (211) x | 1.22 = | 3054.03 (261) |
| Space heating (secondary) | (215) x | 3.07 = | 0 (263) |
| Energy for water heating | (219) x | 1.22 = | 2259.04 (264) |
| Space and water heating | (261) + (262) + (263) + (2 | 264) = | 5313.06 (265) |
| Electricity for pumps, fans and electric kee | ep-hot (231) x | 3.07 = | 230.25 (267) |
| Electricity for lighting | (232) x | 0 = | 1139.7 (268) |
| 'Total Primary Energy | | sum of (265)(271) = | 6683.01 (272) |
| Primary energy kWh/m²/year | | (272) ÷ (4) = | 80.75 (273) |

SAP 2012 Overheating Assessment

Calculated by Stroma FSAP 2012 program, produced and printed on 13 January 2020

Property Details: Plot 104 Dart [Mid] DCC3

| Dwelling type: Located in: Region: Cross ventilation pos Number of storeys: Front of dwelling face Overshading: Overhangs: Thermal mass parame Night ventilation: Blinds, curtains, shut Ventilation rate during Overheating Details: | es: eter: tters: | ather (a | ich): | None Calculated False None | t England st r unknown | | | |
|---|---|---------------------------|--|---|------------------------------|---|--|-------------------------|
| Summer ventilation h Transmission heat lo | | | ient: | 537.48 48.7 | | | | (P1) |
| Summer heat loss co | | | | 48.7 586.18 | | | | (P2) |
| Overhangs: | | | | | | | | |
| Orientation: | Ratio: | | Z_overhangs: | | | | | |
| North West (Front) | 0 | | 1 | | | | | |
| South East (Rear) | 0 | | 1 | | | | | |
| South East (Patio) | 0 | | 1 | | | | | |
| Solar shading: | | | | | | | | |
| | | | | | | | | |
| Orientation: | Z blinc | ls: | Solar access: | Ove | rhangs: | Z summer: | | |
| Orientation: North West (Front) | Z blinc 1 | ls: | Solar access: 0.9 | Ove 1 | rhangs: | Z summer: 0.9 | | (P8) |
| North West (Front) South East (Rear) | 1 1 | ls: | 0.9 0.9 | 1 1 | rhangs: | 0.9 0.9 | | (P8) |
| North West (Front) | | ls: | 0.9 | | rhangs: | 0.9 | | • • |
| North West (Front) South East (Rear) | 1 1 | ls: | 0.9 0.9 | 1 1 | rhangs: | 0.9 0.9 | | (P8) |
| North West (Front) South East (Rear) South East (Patio) | 1 1 | ds: Area | 0.9 0.9 | 1 1 | rhangs: FF | 0.9 0.9 | Gains | (P8) |
| North West (Front) South East (Rear) South East (Patio) Solar gains: | 1 1 | Area | 0.9 0.9 0.9 Flux 105.45 | 1 1 1 | | 0.9 0.9 0.9 | Gains 204.92 | (P8) |
| North West (Front) South East (Rear) South East (Patio) Solar gains: Orientation North West (Front) South East (Rear) | 1 1 1 0.9 x 0.9 x | Area 4.76 3 | 0.9 0.9 0.9 Flux 105.45 126.97 | 1 1 1 g_ 0.72 0.72 | FF 0.7 0.7 | 0.9 0.9 0.9 Shading 0.9 0.9 0.9 | 204.92 155.5 | (P8) |
| North West (Front) South East (Rear) South East (Patio) Solar gains: Orientation North West (Front) | 1 1 1 0.9 x | Area 4.76 | 0.9 0.9 0.9 Flux 105.45 | 1 1 1 g_ 0.72 | FF 0.7 | 0.9 0.9 0.9 Shading 0.9 0.9 0.9 0.9 | 204.92 155.5 270.58 | (P8) (P8) |
| North West (Front) South East (Rear) South East (Patio) Solar gains: Orientation North West (Front) South East (Rear) South East (Patio) | 1 1 1 0.9 x 0.9 x | Area 4.76 3 | 0.9 0.9 0.9 Flux 105.45 126.97 | 1 1 1 g_ 0.72 0.72 | FF 0.7 0.7 | 0.9 0.9 0.9 Shading 0.9 0.9 0.9 | 204.92 155.5 | (P8) |
| North West (Front) South East (Rear) South East (Patio) Solar gains: Orientation North West (Front) South East (Rear) | 1 1 1 0.9 x 0.9 x | Area 4.76 3 | 0.9 0.9 0.9 Flux 105.45 126.97 | 1 1 1 g_ 0.72 0.72 | FF 0.7 0.7 | 0.9 0.9 0.9 Shading 0.9 0.9 0.9 0.9 | 204.92 155.5 270.58 | (P8) (P8) |
| North West (Front) South East (Rear) South East (Patio) Solar gains: Orientation North West (Front) South East (Rear) South East (Patio) | 1 1 1 0.9 x 0.9 x 0.9 x 0.9 x | Area 4.76 3 5.22 | 0.9 0.9 0.9 Flux 105.45 126.97 126.97 | 1 1 1 0.72 0.72 0.72 0.72 0.72 0.72 0.72 | FF 0.7 0.7 | 0.9 0.9 0.9 Shading 0.9 0.9 0.9 0.9 | 204.92 155.5 270.58 631 August 428.31 986.28 1.68 17.5 1.03 20.22 | (P8) (P8) (P3/P4) |